

Transmission Line Modelling, TLM, for System Simulation

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Some Industrial Partners and Applications



*Aircraft
Saab AB*



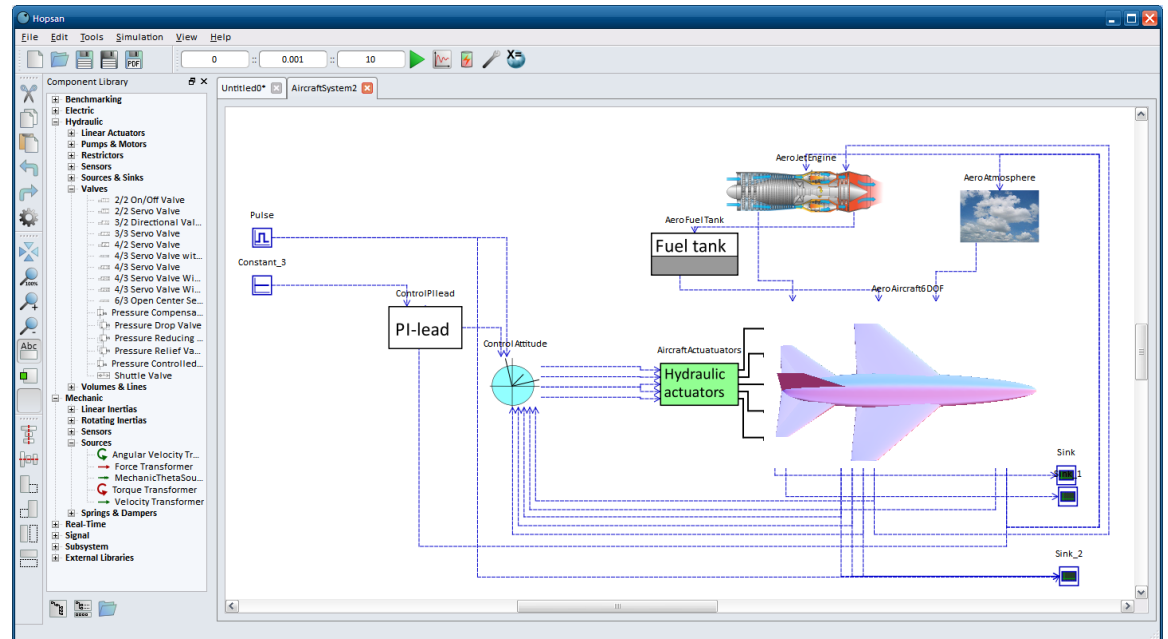
*Construction
Machines
Volvo CE*



*Rock drills
Atlas Copco*

Multi domain dynamic system simulation

- Oil hydraulics
- Gas, pneumatics
- Thermal
- Electrical power
- Mechanical
- Flight dynamics
- Control systems
- Propulsion
- Real systems tend to become very complex and multidisciplinary
- Many systems (e.g. hydraulics) are prone to be numerically stiffness, strong nonlinearities, and discontinuities.

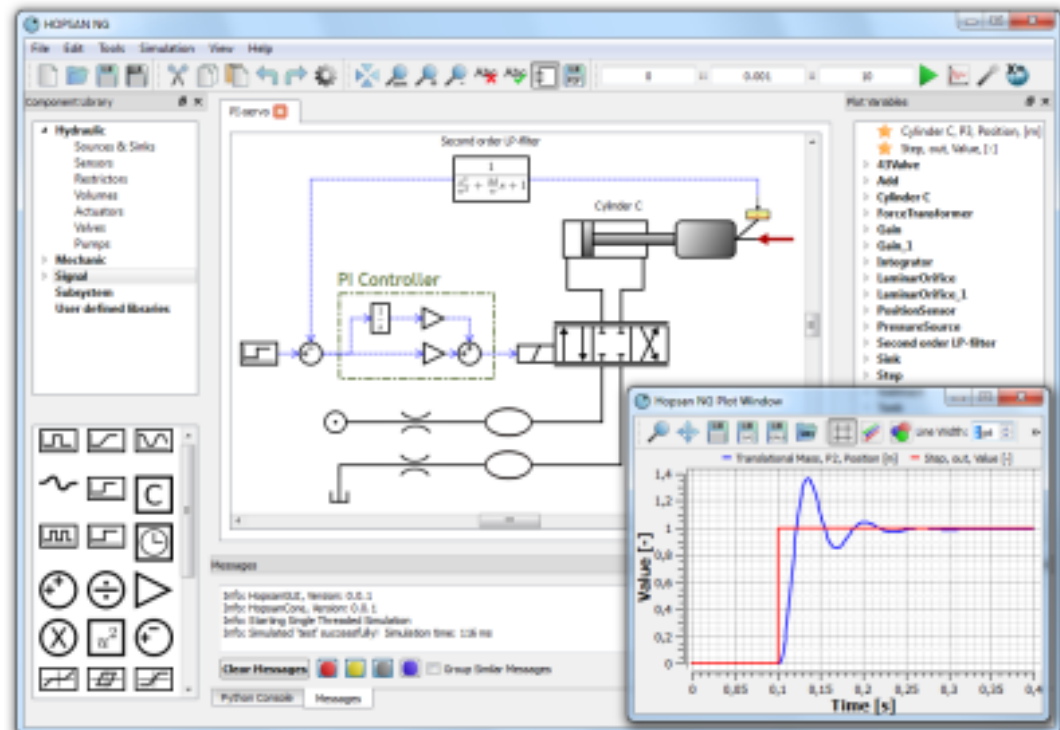


Hopsan Development

- Software for system simulation. Hydraulic, mechanical, electrical, control systems, thermal, etc.
- Work on first Hopsan (in Fortran) began in late 1970s at Linköping University
- Used by industry and for research
- Development of new version called Hopsan NG (in C++) began in 2009
- Longest running simulation software with continuous development *in the world* (?)
- Current version: Beta 0.7
- Open source that can be downloaded from <http://www.iei.liu.se/flumes/system-simulation/hopsanng>

Hopsan NG

- Genuine team work at Flumes
- Freeware that can be downloaded from <http://www.iei.liu.se/flumes/system-simulation/hopsanng>



Bilateral Delay Lines or Transmission Line Modelling (TLM)

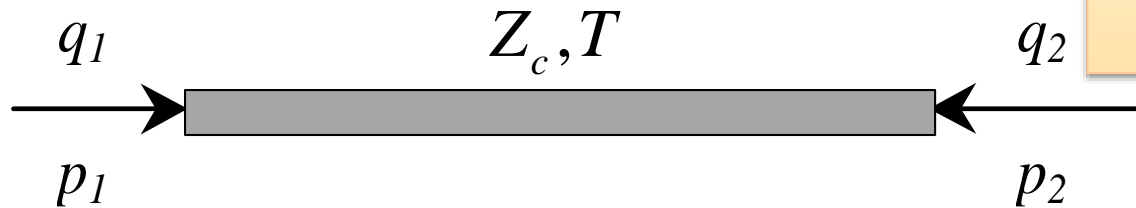
- D M Auslander, 'Distributed System Simulation with Bilateral Delay-Line Models' *Journal of Basic Engineering*, Trans. ASME p195-p200, June 1968.
- P. B. Johns and M.O'Brien. 'Use of the transmission line modelling (t.l.m) method to solve nonlinear lumped networks.' *The Radio Electron and Engineer*. 1980.
- P Krus, A Jansson, J-O Palmberg, K Weddfeldt. 'Distributed Simulation of Hydromechanical Systems'. Presented at 'Third Bath International Fluid Power Workshop', Bath, UK 1990.
- Burton, J. D., Edge, K. A., Burrows, C. R., 1993. Partitioned simulation of hydraulic systems using transmission-line modelling. *In: ASME WAM*, New Orleans, LA, USA. Publ by ASME, New York, NY, USA. (*Using Transputer technology*)

The transmission line

Can represent:

Electrical line, hydraulic line, pneumatic line, spring.

Both capacitance and inductance



$$p_1(t) = p_2(t - T) + Z_c (q_1(t) + q_2(t - T))$$

$$p_2(t) = p_1(t - T) + Z_c (q_2(t) + q_1(t - T))$$

Alternatively

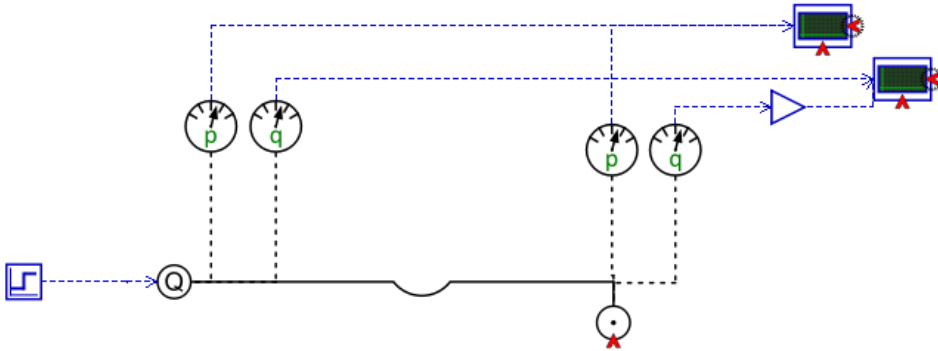
$$p_1(t) = c_1(t) + Z_c q_1(t)$$

$$c_1(t) = p_2(t - T) + Z_c q_2(t - T)$$

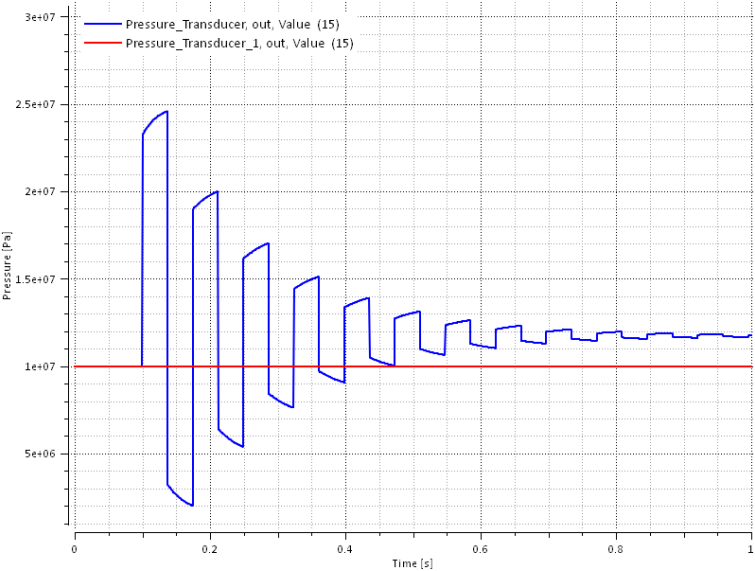
$$p_2(t) = c_2(t) + Z_c q_2(t)$$

$$c_2(t) = p_1(t - T) + Z_c q_1(t - T)$$

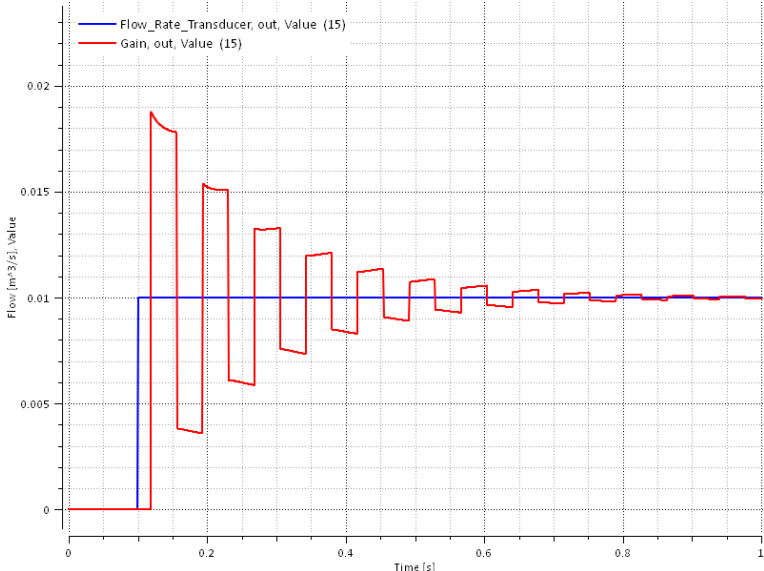
Simulation of long transmission line



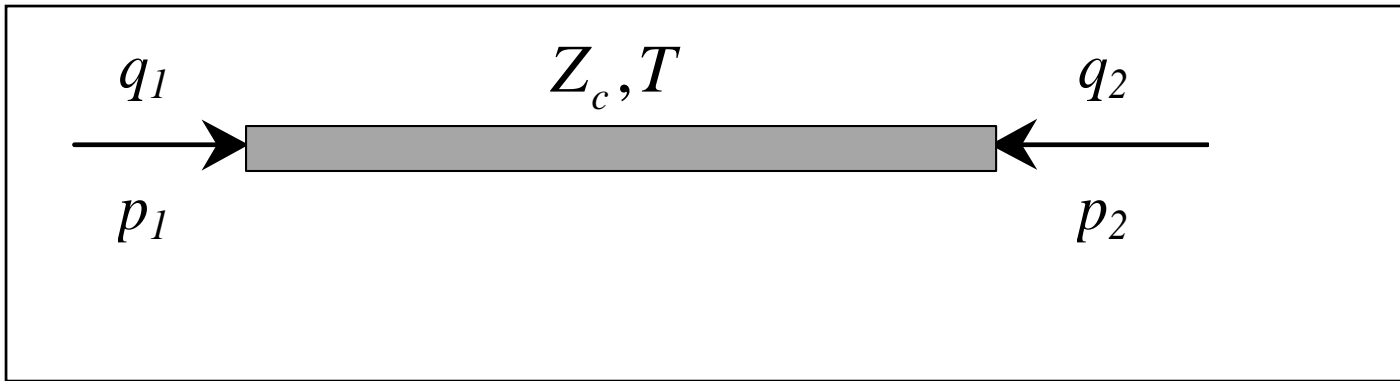
Pressure



Flows



The transmission line



Capacitance and inductance as a function of characteristic impedance and delay time

$$C = \frac{T}{Z_c}$$
$$L = Z_c T$$
$$Z_c = \sqrt{\frac{L}{C}}$$
$$T = \sqrt{LC}$$

If time step and capacitance are known

$$Z_c = \frac{T}{C}$$
$$L_p = \frac{T^2}{C}$$

Parasitic inductance

If time step and inductance are known

$$Z_c = \frac{L}{T}$$
$$C_p = \frac{T^2}{L}$$

Parasitic capacitance

Block Diagram

$$c_1(t) = p_2(t - T) + Z_c q_2(t - T)$$

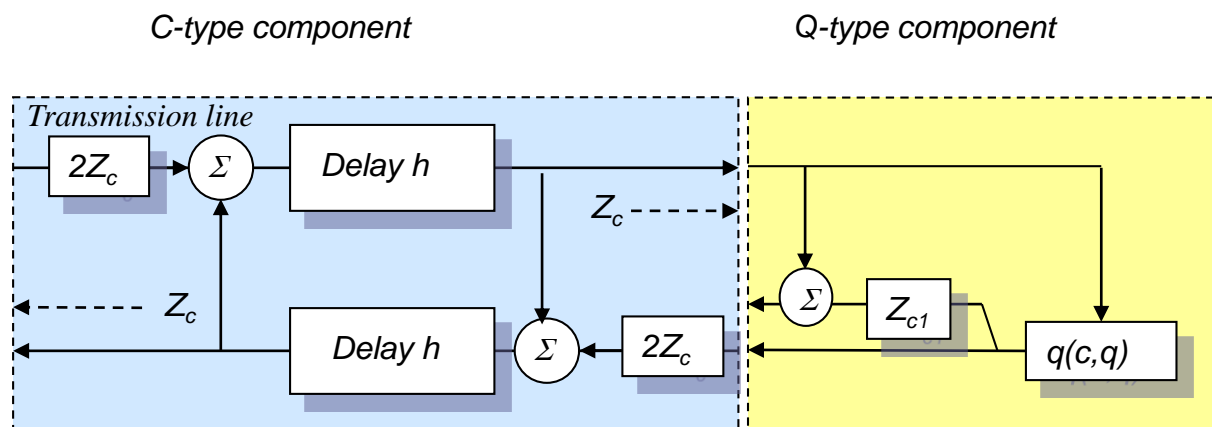
$$c_2(t) = p_1(t - T) + Z_c q_1(t - T)$$

$$p_1(t) = c_1(t) + Z_c q_1(t)$$

$$p_2(t) = c_2(t) + Z_c q_2(t)$$

$$c_1(t) = c_2(t - T) + 2Z_c q_2(t - T)$$

$$c_2(t) = c_1(t - T) + 2Z_c q_1(t - T)$$

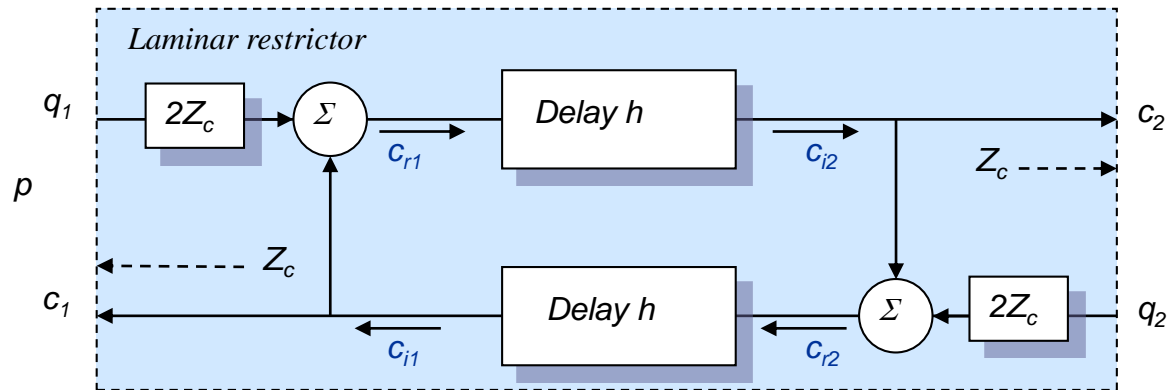
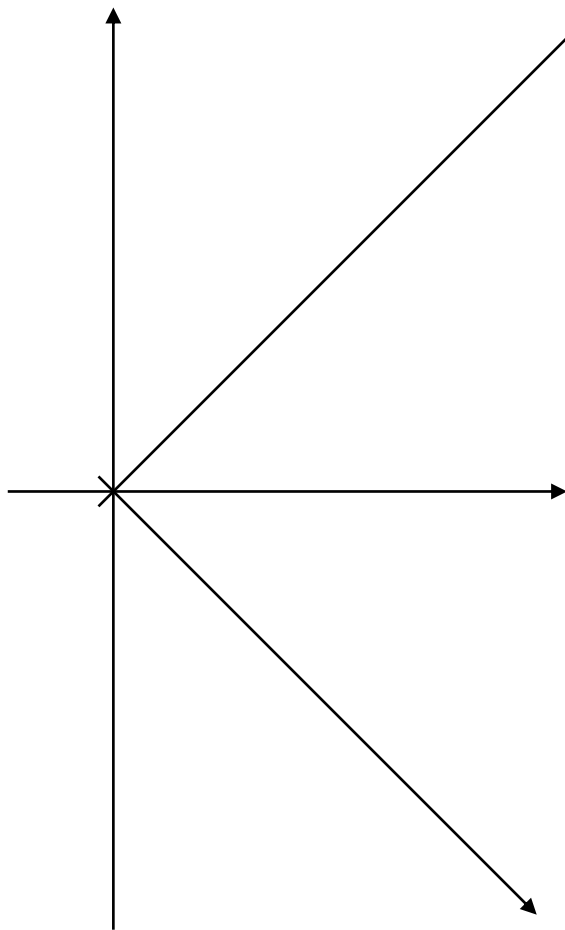


Relations between p , q and c_i , c_r

$Z_c q$

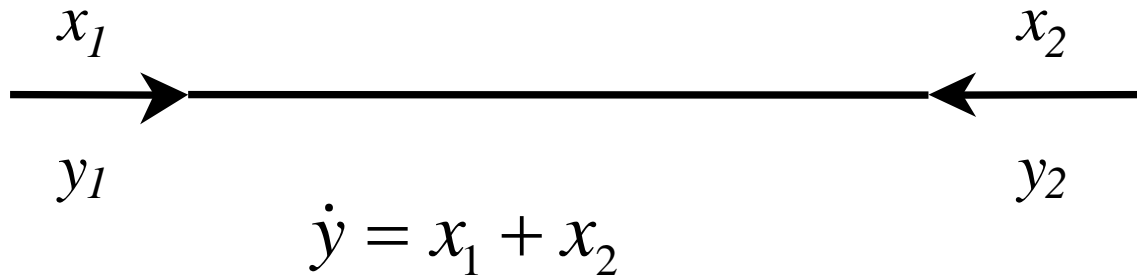
$$c_r = p + Z_c q$$

$$(c_r = \frac{1}{\sqrt{Z_c}} p + \sqrt{Z_c} q)$$



$$c_i = p - Z_c q$$

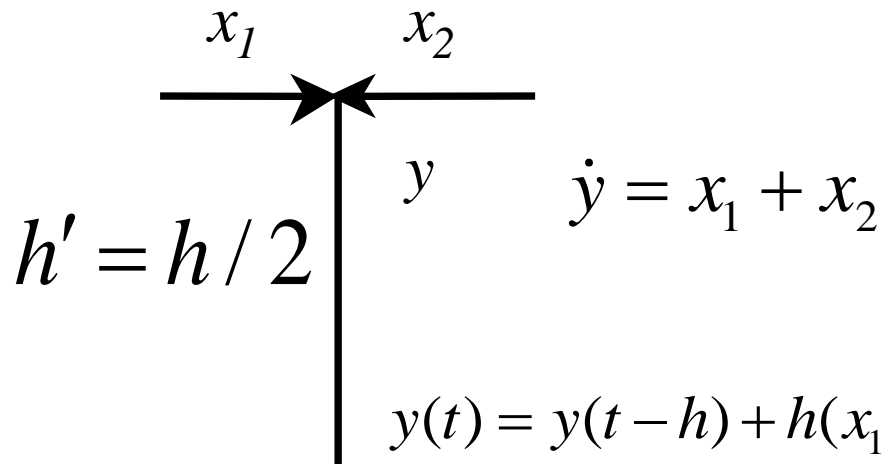
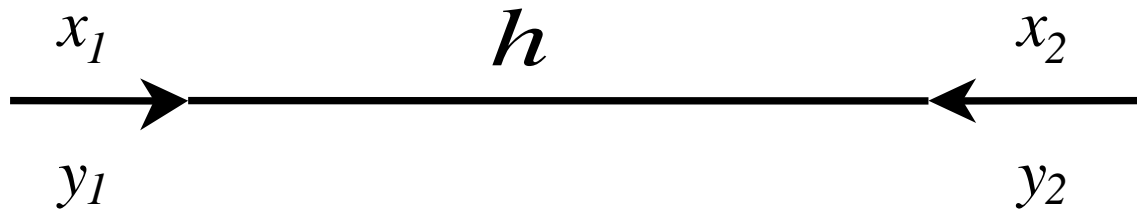
The Transmission Line as a General Integrator



$$y_1(t) = y_2(t - T) + h(x_1(t) + x_2(t - T))$$

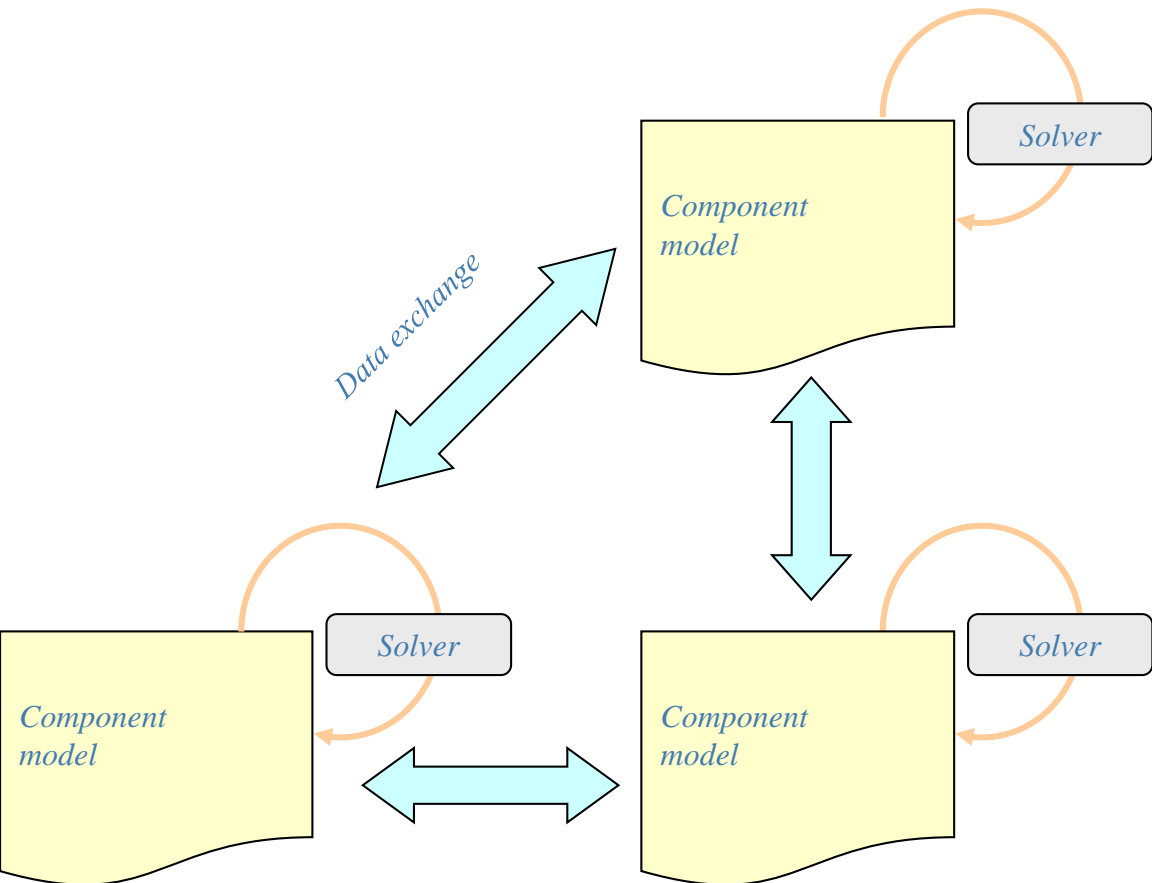
$$y_2(t) = y_1(t - T) + h(x_2(t) + x_1(t - T))$$

The Trapezoidal Rule as an Integrator



$$y(t) = y(t-h) + h(x_1(t) + x_2(t) + x_1(t-h) + x_2(t-h))$$

Distributed Model Structure



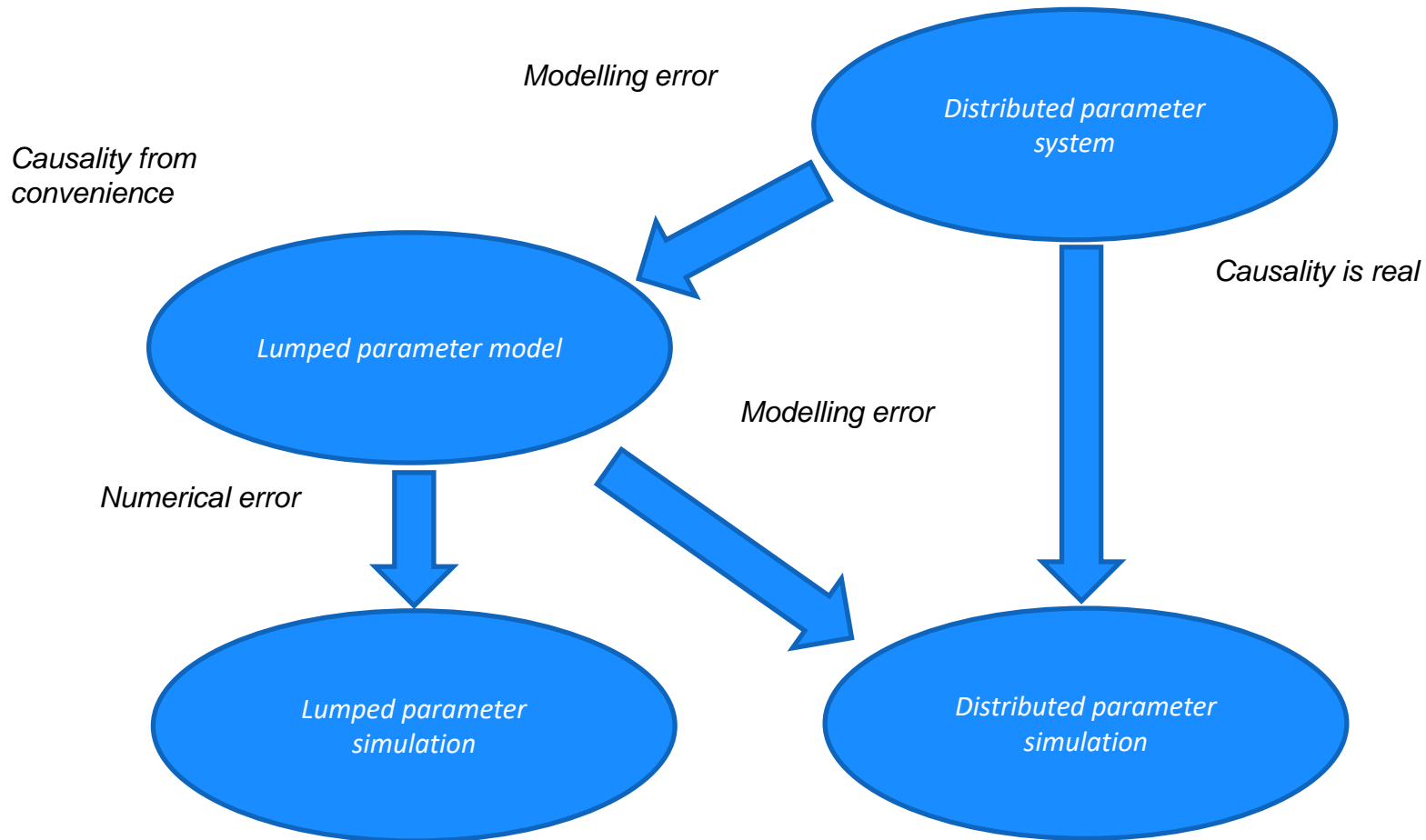
Individual simulation set-up

Ideal for using multi-core architectures

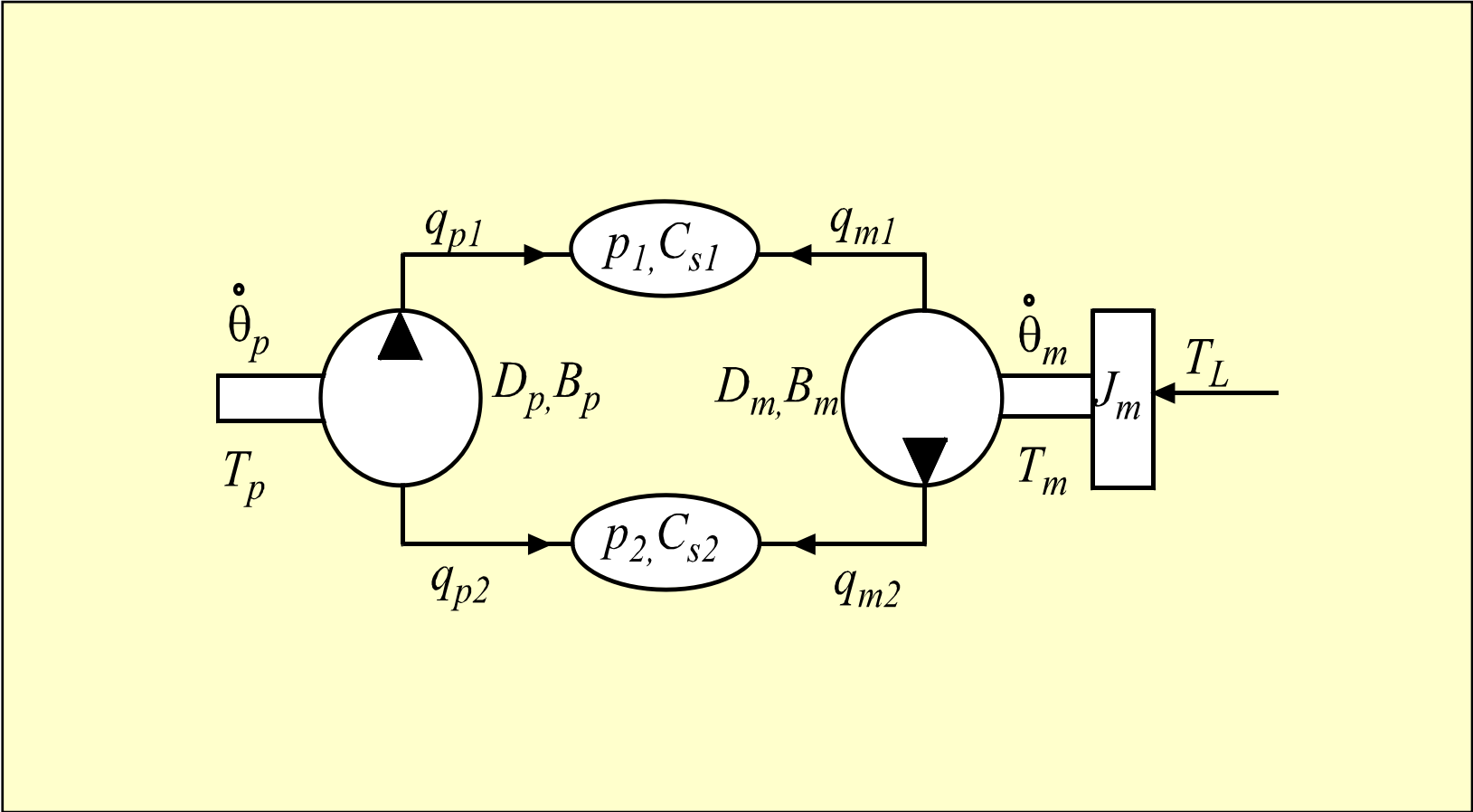
Enables interdisciplinary model development and simulation

Efficient for large systems

Relations between distributed and lumped parameter modelling



Example: Pump-motor system



F(y,dy/dt) and y for the transmission

$$F(y, \dot{y}, u, t) = \begin{pmatrix} \dot{\theta}_p B_p + \frac{p_a - p_b}{D_p} - T_p \\ -\dot{\theta}_p D_p + q_{p1} \\ \dot{\theta}_p D_p + q_{p2} \\ \dot{p}_1 - \frac{q_{m1} + q_{p1}}{C_{s1}} \\ \dot{p}_2 - \frac{q_{m2} + q_{p2}}{C_{s2}} \\ -\dot{\theta}_m D_m + q_{m1} \\ \dot{\theta}_m D_m + q_{m2} \\ -\dot{\theta}_m B_m + \frac{p_a - p_b}{D_m} - T_m \\ \ddot{\theta}_m + \frac{B_m}{J_m} \dot{\theta}_m - \frac{p_a - p_b}{J_m D_m} + \frac{T_L}{J_m} \end{pmatrix}$$

$$y = \begin{pmatrix} T_p \\ q_{p1} \\ q_{p2} \\ p_1 \\ p_2 \\ q_{m1} \\ q_{m2} \\ T_m \\ \theta_m \end{pmatrix}$$

Differential algebraic equations

$$F(x, \dot{x}, u, t) = 0$$

$$F\left(y, \frac{dy}{dt}, \frac{d^2y}{dt^2}, \dots, \frac{d^2y}{dt^2}, t\right) = 0$$

$$\frac{d}{dt} = \frac{2(1 - q^{-1})}{h(1 + q^{-1})}$$

Bilinear transform (derived from the trapezoidal rule, second order Runge-Kutta)

$$qy = y(t + h)$$

q is the time displacement operator

Differential algebraic equations

$$F\left(y, \frac{dy}{dt}, \frac{d^2y}{dt^2}, \dots, \frac{d^2y}{dt^2}, t\right) = 0$$

can be transformed into:

$$G(y(t), y(t-h), \dots, y(t-nh), u(t), u(t-h), \dots, u(t-nh), t) = 0$$

$$G(y(t), t) = 0$$

Use Newton-Rapson

$$y_{k+1} = y_k(t) - J_k(t)^{-1} G(y_k(t))$$

$$J_{ijk} = \frac{\partial G_i(y_k(t))}{\partial y_j}$$

Compare: Differential algebraic equations with lumped parameters

$G(y, t) =$

$$\left(\begin{array}{l}
 \text{DS}[1, -h p_a + h p_b + D_p (h T_p + 2 B_p \theta_p)] - h p_a + h p_b + h D_p T_p - 2 B_p D_p \theta_p \\
 \text{DS}[1, h q_{p1} + 2 D_p \theta_p] + h q_{p1} - 2 D_p \theta_p \\
 \text{DS}[1, h q_{p2} - 2 D_p \theta_p] + h q_{p2} + 2 D_p \theta_p \\
 \text{DS}[1, -2 C_{s1} p_a - h (q_{m1} + q_{p1})] + 2 C_{s1} p_a - h (q_{m1} + q_{p1}) \\
 \text{DS}[1, -2 C_{s2} p_b + h (q_{m2} + q_{p2})] + 2 C_{s2} p_b + h (q_{m2} + q_{p2}) \\
 \text{DS}[1, h q_{m1} - 2 D_m \theta_m] + h q_{m1} + 2 D_m \theta_m \\
 \text{DS}[1, h q_{m2} + 2 D_m \theta_m] + h q_{m2} - 2 D_m \theta_m \\
 \text{DS}[1, -h p_a + h p_b + D_m (h T_m - 2 B_m \theta_m)] - h p_a + h p_b + h D_m T_m + 2 B_m D_m \theta_m \\
 \text{DS}[1, 2(-k^2 p_a + k^2 p_b + D_m (k^2 T_L - 4 J_m \theta_m))] + \text{DS}[2, -k^2 p_a + k^2 p_b + D_m (k^2 T_L - \\
 2 h B_m \theta_m + 4 J_m \theta_m)] - k^2 p_a + k^2 p_b + k^2 D_m T_L + 2 h B_m D_m \theta_m + 4 D_m J_m \theta_m
 \end{array} \right)$$

Jacobian of the lumped time discrete algebraic system

$$J = \begin{pmatrix} h D_p & 0 & 0 & -h & h & 0 & 0 & 0 & 0 \\ 0 & h & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & h & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & -h & 0 & 2 C_{s1} & 0 & -h & 0 & 0 & 0 \\ 0 & 0 & h & 0 & 2 C_{s2} & 0 & h & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & h & 0 & 0 & 2 D_m \\ 0 & 0 & 0 & 0 & 0 & 0 & h & 0 & -2 D_m \\ 0 & 0 & 0 & -h & h & 0 & 0 & h D_m & 2 B_m D_m \\ 0 & 0 & 0 & -h^2 & h^2 & 0 & 0 & 0 & 2 h B_m D_m + 4 D_m J_m \end{pmatrix}$$

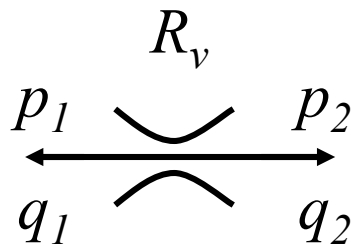
Time discrete algebraic system with distributed parameters

$$G(y, t) = \begin{pmatrix} \text{DS}[1, -h p_a + h p_b + D_p (h T_p + 2 B_p \theta_p)] - h p_a + h p_b + h D_p T_p - 2 B_p D_p \theta_p \\ \text{DS}[1, h q_{p1} + 2 D_p \theta_p] + h q_{p1} - 2 D_p \theta_p \\ \text{DS}[1, h q_{p2} - 2 D_p \theta_p] + h q_{p2} + 2 D_p \theta_p \\ -\text{DS}[1, p_{a2}] + p_{a1} + (\text{DS}[1, q_{m1}] - q_{p1}) Z_c \\ -\text{DS}[1, p_{b2}] + p_{b1} + (\text{DS}[1, q_{m2}] - q_{p2}) Z_c \\ -\text{DS}[1, p_{a1}] + p_{a2} + (\text{DS}[1, q_{p1}] - q_{m1}) Z_c \\ -\text{DS}[1, p_{b1}] + p_{b2} + (\text{DS}[1, q_{p2}] - q_{m2}) Z_c \\ \text{DS}[1, h q_{m1} - 2 D_m \theta_m] + h q_{m1} + 2 D_m \theta_m \\ \text{DS}[1, h q_{m2} + 2 D_m \theta_m] + h q_{m2} - 2 D_m \theta_m \\ \text{DS}[1, -h p_a + h p_b + D_m (h T_m - 2 B_m \theta_m)] - h p_a + h p_b + h D_m T_m + 2 B_m D_m \theta_m \\ \text{DS}[1, 2(-h^2 p_a + h^2 p_b + D_m (h^2 T_L - 4 J_m \theta_m))] + \text{DS}[2, -h^2 p_a + h^2 p_b + \\ D_m (h^2 T_L - 2 h B_m \theta_m + 4 J_m \theta_m)] - h^2 p_a + h^2 p_b + h^2 D_m T_L + \\ 2 h B_m D_m \theta_m + 4 D_m J_m \theta_m \end{pmatrix}$$

Jacobian of the distributed time discrete algebraic system

$$J = \begin{pmatrix} h D_p & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & h & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & h & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & -Z_c & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & -Z_c & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & -Z_c & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & -Z_c & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & h & 0 & 0 & 2 D_m \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & h & 0 & -2 D_m \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & h D_m & 2 B_m D_m \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 2 h B_m D_m + 4 J_m D_m \end{pmatrix}$$

Laminar restrictor with transmission line boundaries



From transmission line

$$q_2 = \frac{p_1 - p_2}{R_v}$$

$$q_1 = -q_2$$

$$p_1 = c_1 + Z_c q_1$$

$$p_2 = c_2 + Z_c q_2$$

Solved for p_1 and p_2

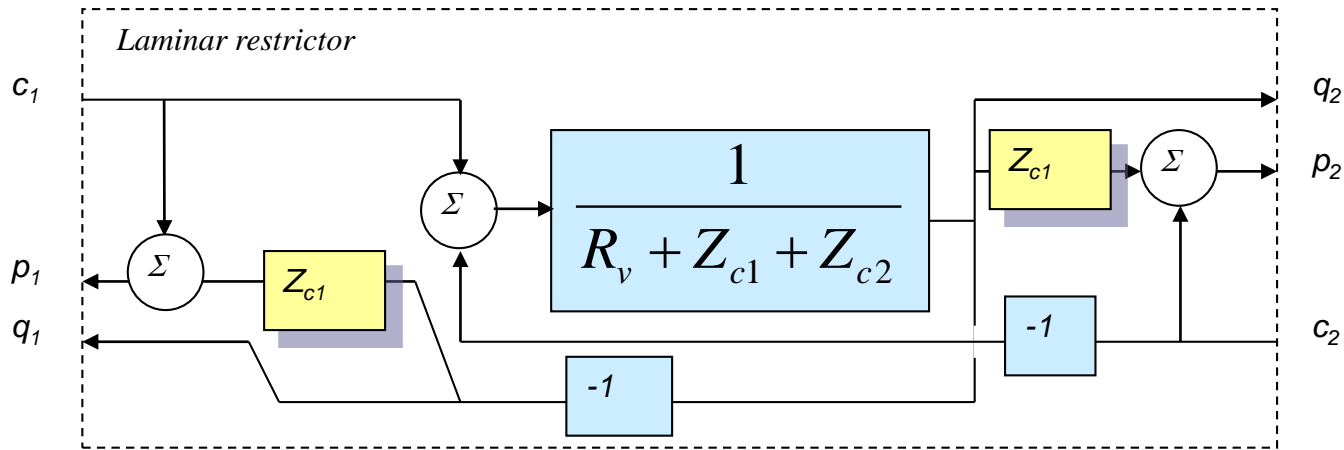
$$q_2 = \frac{c_1 - c_2}{R_v + Z_{c1} + Z_{c2}}$$

$$q_1 = -q_2$$

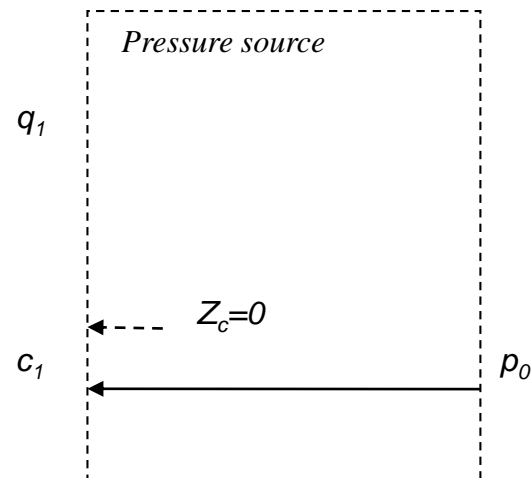
$$p_1 = c_1 + Z_c q_1$$

$$p_2 = c_2 + Z_c q_2$$

Blockdiagram of laminar restrictor



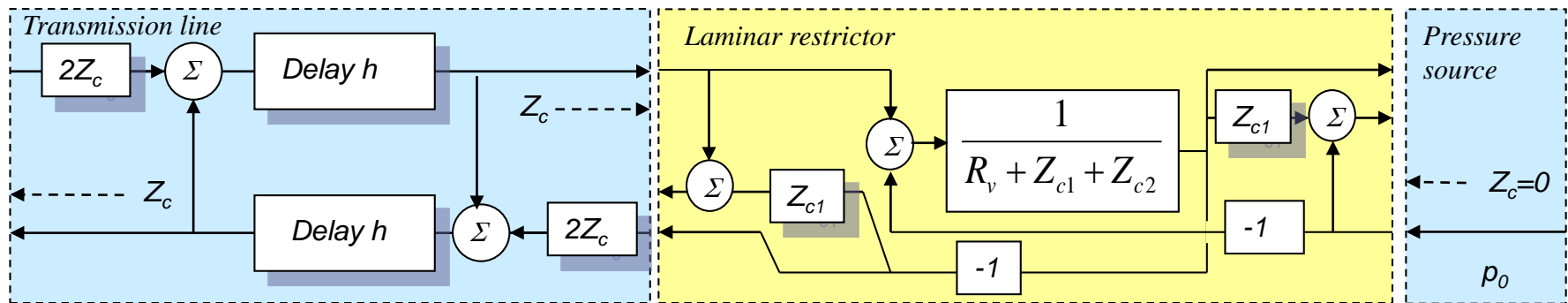
Blockdiagram of pressure source



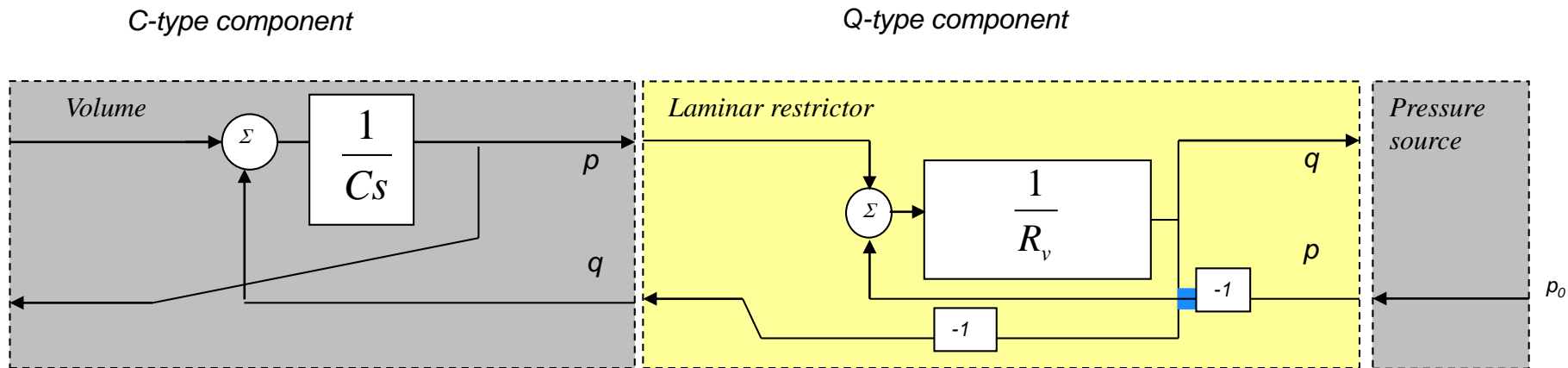
Blockdiagram of orifice connected to a line and a pressure source

C-type component

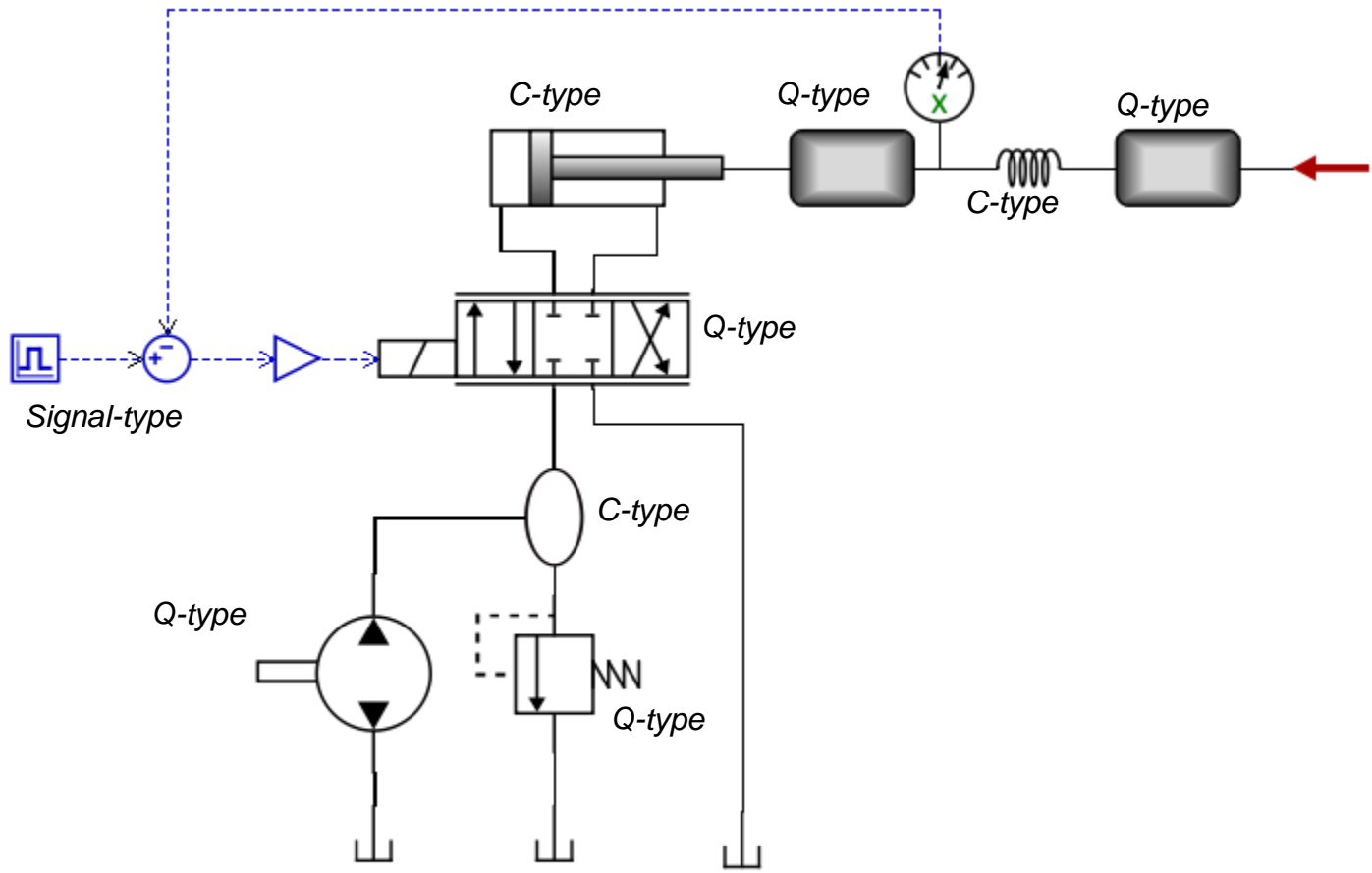
Q-type component



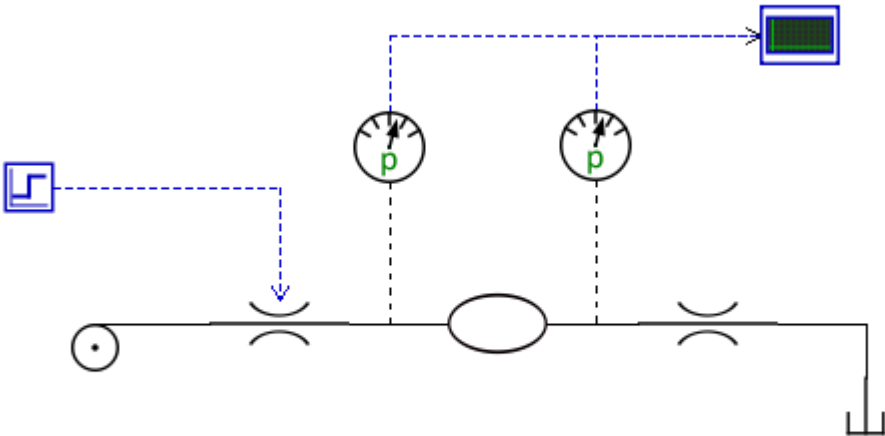
Blockdiagram of orifice connected to a line and a pressure source (lumped parameters)



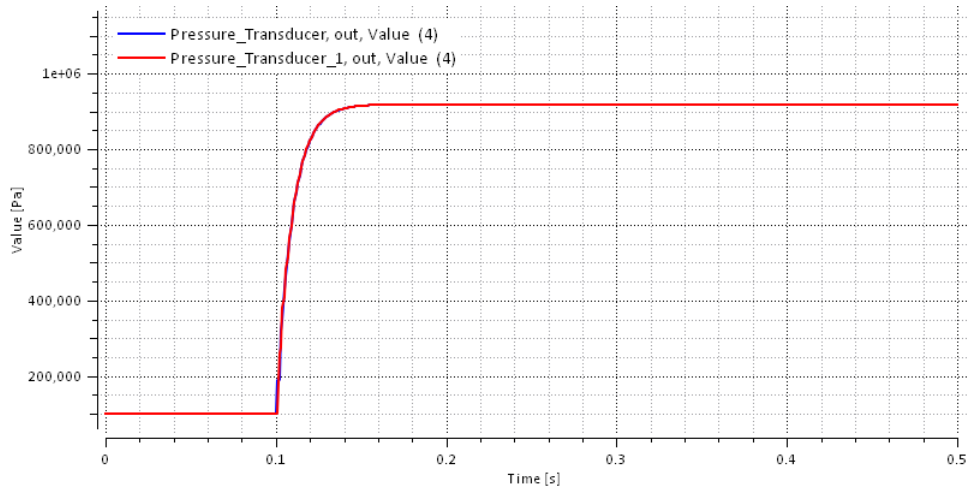
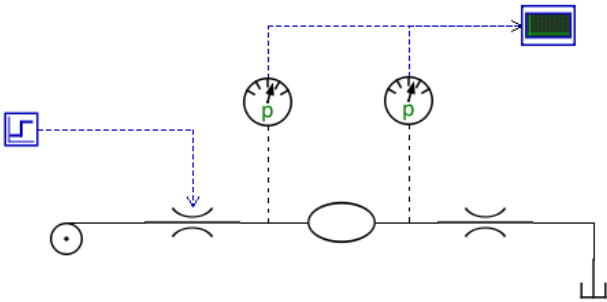
Example



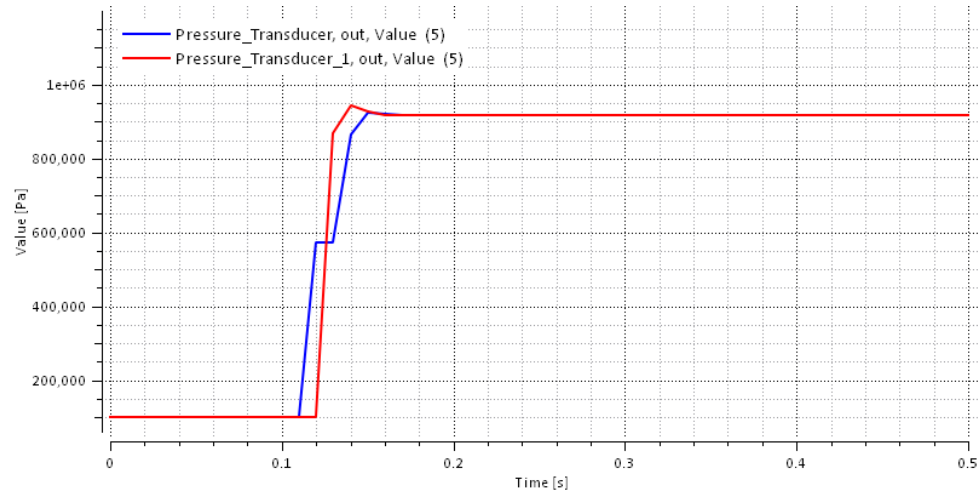
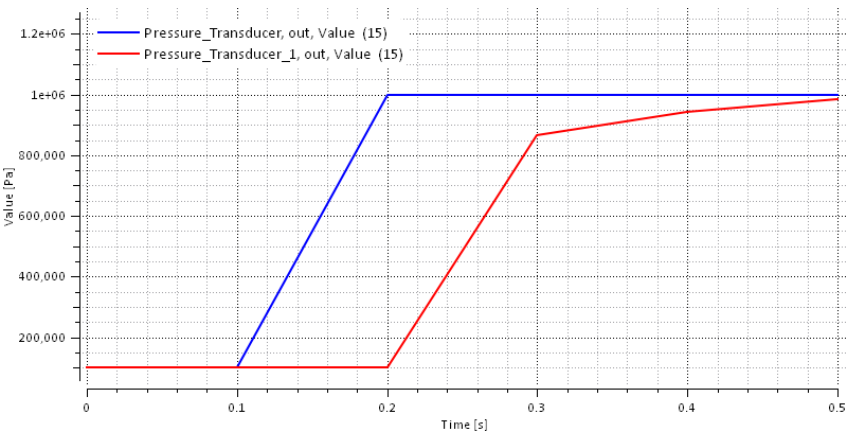
Example



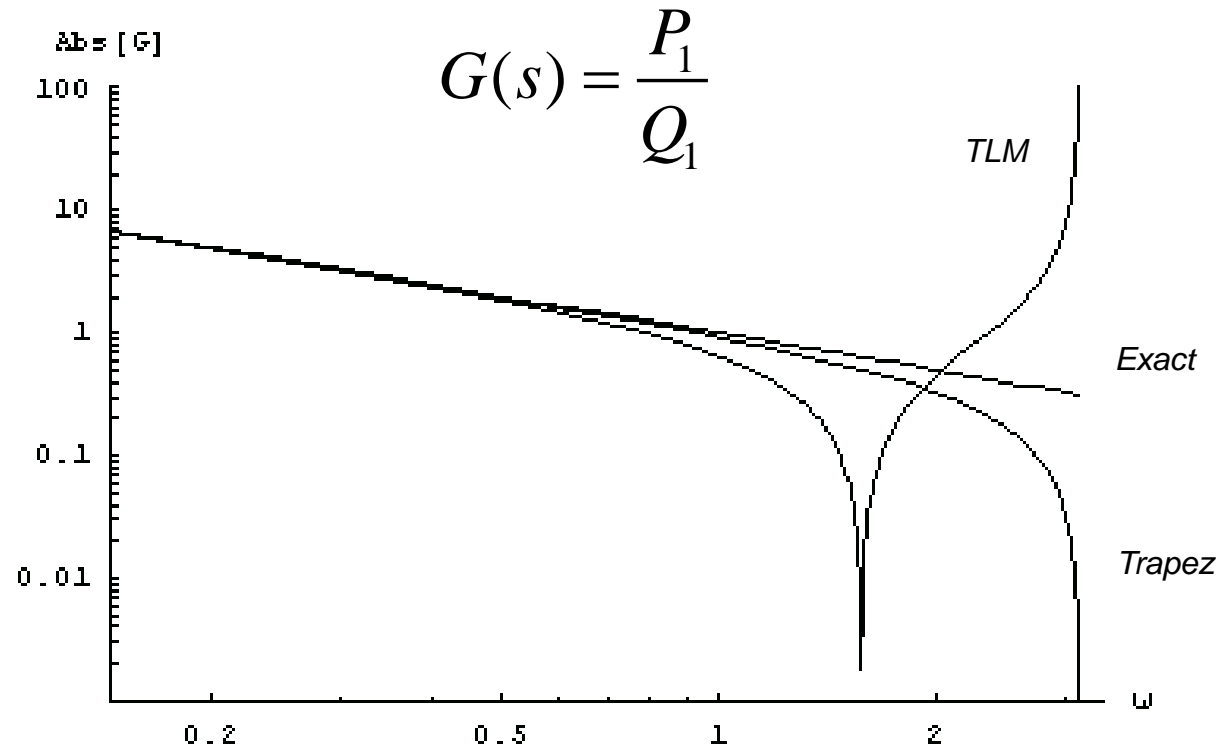
Example



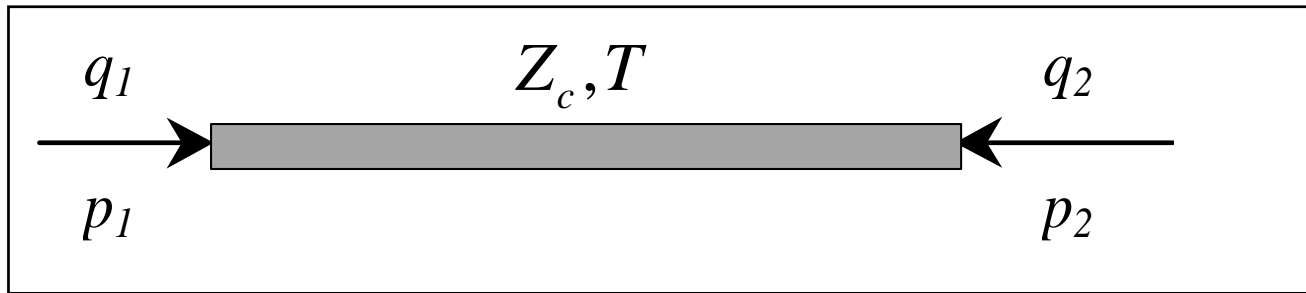
Pressure with times step $h=0.001, 0.01, 0.1$ [s]



Bode diagram of TLM element with blocked end at 2 and the trapezoidal rule



Filtering of wave variable to suppress high frequency oscillations



$$p_1(t) = c_1(t) + Z_c q_1(t)$$

$$c_1(t) = p_2(t - T) + Z_c q_2(t - T)$$

$$p_2(t) = c_2(t) + Z_c q_2(t)$$

$$c_2(t) = p_1(t - T) + Z_c q_1(t - T)$$

$$p_1(t) = c_{f1}(t) + Z_c q_1(t)$$

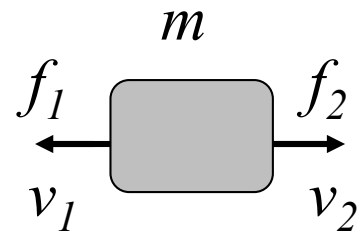
$$c_{f1}(t) = \alpha c_{f1}(t - T) + (1 - \alpha) c_1(t)$$

$$p_2(t) = c_{f2}(t) + Z_c q_2(t)$$

$$c_{f2}(t) = \alpha c_{f2}(t - T) + (1 - \alpha) c_2(t)$$

$$\alpha \approx [0.05, 0.5]$$

Mass with transmission line boundaries



$$\dot{v}_2 = \frac{f_1 - f_2}{m} - b\dot{v}_2$$

$$v_1 = -v_2$$

$$\dot{x}_2 = v_2$$

$$x_1 = -x_2$$

$$f_1 = c_{x1} + Z_{cx} v_1$$

$$f_2 = c_{x2} + Z_{cx} v_2$$

From transmission line

Solved for f_1 and f_2

$$\dot{v}_2 = \frac{c_{x1} - c_{x2}}{m} - (b + Z_{c1} + Z_{c2})v_2$$

$$v_1 = -v_2$$

$$x_2 = \frac{v_2}{s}$$

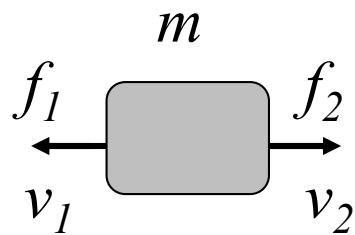
$$x_1 = -x_2$$

$$f_1 = c_{x1} + Z_{cx} v_1$$

$$f_2 = c_{x2} + Z_{cx} v_2$$

Mass with transmission line boundaries

Can be solved using bilinear transform $s \rightarrow \frac{2}{h} \frac{1-q^{-1}}{1+q^{-1}}$



$$V_2 = \frac{F_1 - F_2}{ms + b}$$

$$V_1 = -V_2$$

$$X_2 = \frac{V_2}{s}$$

$$X_1 = -X_2$$

Solved for F_1 and F_2

$$V_2 = \frac{C_{x1} - C_{x2}}{ms + b + Z_{c1} + Z_{c2}}$$

$$V_1 = -V_2$$

$$X_2 = \frac{V_2}{s}$$

$$X_1 = -X_2$$

$$F_1 = C_{x1} + Z_{cx} V_1$$

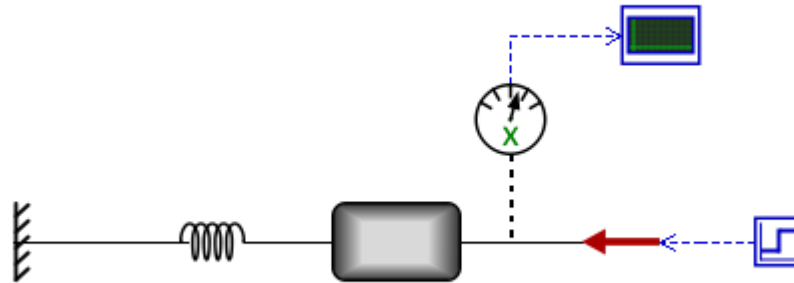
$$F_2 = C_{x2} + Z_{cx} V_2$$

From transmission line

$$F_1 = C_{x1} + Z_{cx} V_1$$

$$F_2 = C_{x2} + Z_{cx} V_2$$

Mass Spring System



Parameters

$$m = 100 \text{ [kg]}$$

$$k = 1000 \text{ [N/m]}$$

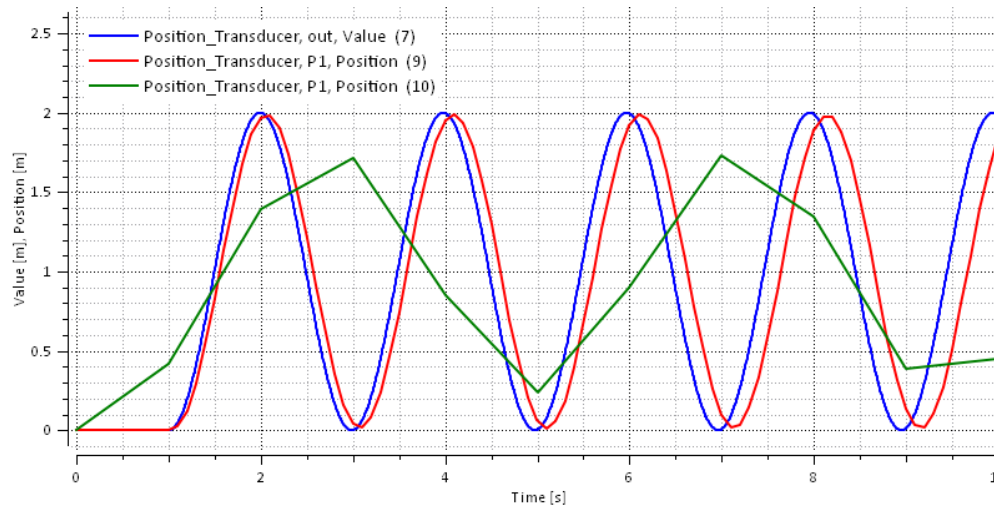
Parasitic mass

$$m_p = kh^2$$

$$m_p = 1000 \times 0.001^2 = 0.001 \text{ [kg]}$$

$$m_p = 1000 \times 0.1^2 = 10 \text{ [kg]}$$

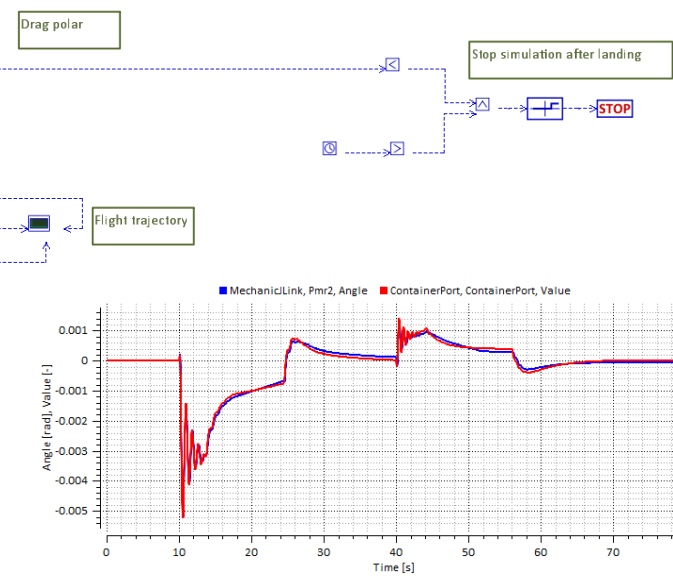
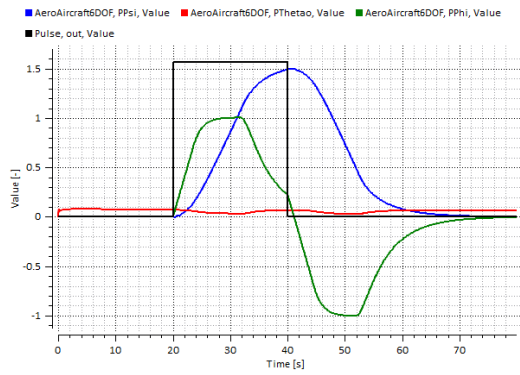
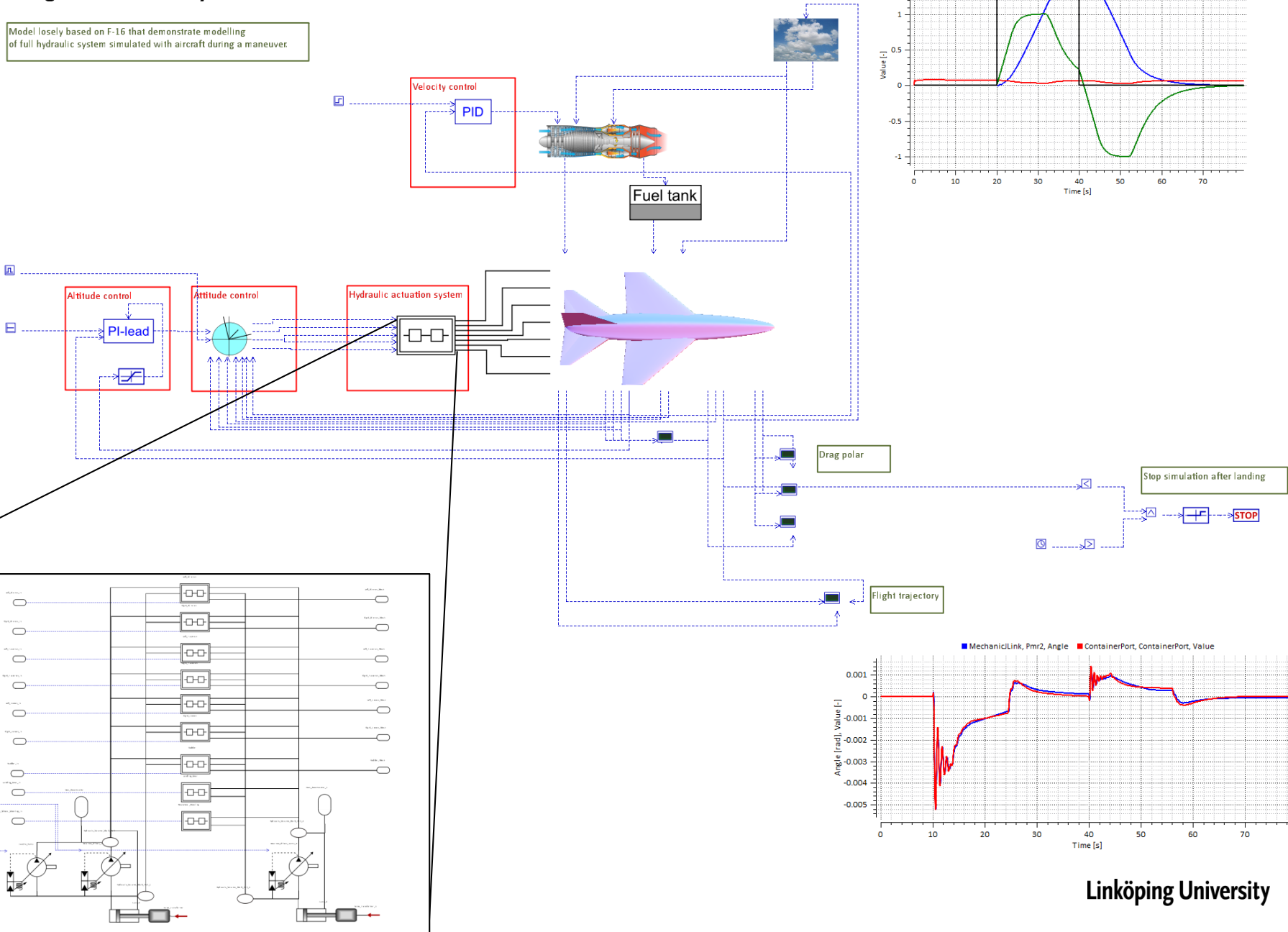
$$m_p = 1000 \times 1^2 = 1000 \text{ [kg]}$$



Position with times step $h=0.001, 0.1, 1$ [s]

Integrated Aircraft System Simulation

Model loosely based on F-16 that demonstrate modelling of full hydraulic system simulated with aircraft during a maneuver.





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